



11 Publication number:

0 556 748 A2

(12)

EUROPEAN PATENT APPLICATION

21) Application number: 93102257.8

(51) Int. Cl.5: G01N 15/14

② Date of filing: 12.02.93

Priority: 20.02.92 JP 33441/92
 24.02.92 JP 36262/92
 24.12.92 JP 344578/92

Date of publication of application:25.08.93 Bulletin 93/34

Designated Contracting States:
 AT BE CH DE DK ES FR GB GR IE IT LI LU NL
PT SE

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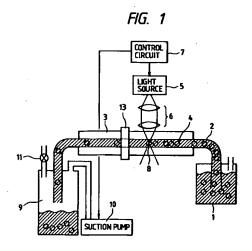
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- Method and apparatus for particle manipulation, and measuring apparatus utilizing the same.
- A flow of liquid containing floating fine particles is formed in a flow path, thereby causing successive movement of the particles. A light beam having intensity distribution from a laser is focused on the liquid flow, whereby the particle is optically trapped at the irradiating position, thus being stopped against the liquid flow or being slowed by a braking force. This phenomenon is utilized in controlling the spacing of the particles in the flow or in separating the particles.



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BACKGROUND OF THE INVENTION

Field of th Inv ntion

The present inv ntion r lates to a technology for manipulating movement of particles in a medium.

Related Background Art

Sheath flow method is already well known for transporting fine particles dispersed in a medium such as liquid, in linear array one by one. In this method, at the center of a high-speed sheath liquid flow, there is formed a very fine flow of liquid in which fine particles such as blood cells, viruses, microorganisms or carrier particles (such as latex particles or ceramic particles) are suspended, whereby the fine particles are separated one by one transported in linear array. Such sheath flow method is applied to so-called flow cytometry which is used for counting the number of such fine particles by optical or electrical method or for identifying the sort or property of such particles by statistical processing of a number of thus obtained data.

On the other hand, for classifying the fine particles by size or specific gravity thereof, there are known methods utilizing the centrifugal force or the sieving means such as meshes or gels. These m thods are applied to classify copying toner or other industrial particles, or to separate microorganisms, cells or the like.

Apart from these technologies, it is already known that, when fine particles are irradiated with a light beam having intensity gradient such as Gaussian laser beam, the particles are subjected to scattering and gradient forces of radiation pressure so that the fine particles are moved in the direction of irradiation by an axial force and are trapped in the light beam by a radial force. This is a technology called optical trapping, disclosed, for example, in Japanese Patent Laid-Open Application Nos. 2-91545 and 3-223645 and in U.S. Patent No. 3,808,550. Also, U.S. Patent No. 4,887,721 discloses a method of switching two crossing laser beams, thereby transporting the fine particles to a pr determined position by laser optical pressure.

SUMMARY OF THE INVENTION

In consideration of the foregoing, the present invention is to provide a novel method for manipulating particl s in a medium. A mor specific object of the present invention is to provide novel method and apparatus for continuously transporting particles in an array with a desired interval. Another more specific object of the present invention is to

provid novel m thod and apparatus for separating particles different in size or in r fractive index.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a view showing the configuration of an apparatus constituting a first embodiment of the present invention:

Fig. 2 is a view showing a part of the configuration of an apparatus of a second embodiment;

Fig. 3 is a view showing the configuration of an apparatus of a third embodiment;

Figs. 4A to 4E are views showing the mode of function of micropump;

Fig. 5 is a view showing the configuration of an apparatus of a fourth embodiment;

Fig. 6 is a view showing the configuration of a measuring system in the apparatus shown in Fig. 5;

Fig. 7 is a view showing the configuration of an apparatus of a fifth embodiment;

Fig. 8 is a schematic view of a sixth embodiment;

Fig. 9 is a schematic view of a seventh embodiment;

Fig. 10 is a schematic view of an eighth embodiment;

Fig. 11 is a schematic view of a ninth embodiment;

Fig. 12 is a schematic view of a tenth embodiment;

Fig. 13 is a schematic view of an eleventh embodiment;

Figs. 14A and 14B are schematic views of the eleventh embodiment;

Fig. 15 is a schematic view of a twelfth embodiment; and

Figs. 16A to 16C are schematic views of the twelfth embodiment.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[1st embodiment]

Fig. 1 is a view showing the configuration of an apparatus constituting a first embodiment of the present invention, wherein a supply container 1 contains therein dispersion of fine particles, consisting of a plurality of fine particles (for example, blood cells, viruses, microorganisms, bioparticles such as DNA or RNA, carrier particles or industrial particles) and dispersion medium. The fine particle s and th dispersion medium hav comparabl specific graviti s. In the mbodiment th fin particles are latex particles of a giv n size while the dispersion m dium is wat r. Th supply contain r 1 is connected to a flow path 2, which is provided

with a flow cell 3 of quartz glass in the middl and connected to a discharge container 9. A vacuum pump 10 and a valv 11 ar connect d to th discharge container 9. The vaccum pump 10 is constantly operated to generate a low pressur in the discharge container 9, thereby creating a flow of particle dispersion of a constant velocity in the flow path 2. The fine particles 4 in the dispersion medium move together with the flow. The internal diameter of the flow path 2 has to be larger than the diameter of the largest particle, but preferably does not exceed twice of the diameter of the largest particle, since an excessively large internal diameter increases the possibility of simultaneous flowing of plural particles.

A light source 5, positioned above the flow cell 3, generates a light beam of a predetermined intensity gradient for optical trapping, and is so selected that the wavelength thereof is in a low optical absorption band of the particles. In the present mbodiment there is employed a TEMoo mode of YAG laser to generate a Gaussian beam, but there may also be employed various lasers such as solid-state laser, gas laser or semiconductor laser, or light sources not limited to laser, capable of generating light having intensity gradient. The light beam emitted by the light source 5 is focused by a lens system 6 to a position 8 in the flow path in the flow cell 3. A control means 7 controls the light source 5 itself or light control means (such as a shutter or a light modulating element) separate from the light source 5, thereby effecting on-off control or intensity modulation of the light irradiation on the irradiation position 8. The control means 7 also sends instruction to the vacuum pump 10. At a downstream side of the irradiation position 8 in the flow cell 3, there is provided particle measuring means 13 utilizing, for example, optical, electrical, magnetic or acoustooptical method.

When the fine particle passes the irradiation position 8 while the light beam is focused thereon, the fine particle is subjected to two forces, namely, an axial force toward the irradiating direction of the light beam, and a radial force to confine the particle in the optical axis. Each of the forces depends on the intensity of the laser beam and the intensity distribution along the optical axis, namely, degree of condensation by the lens and the intensity distribution in a direction perpendicular to the optical axis. They also depend on the refractive index and absorbance (reflectance) of the particle, and on the particle size. By means of the radial force, the fine particle may be stopped by trapping at the irradiation position 8, or the moving velocity of the particl may be t mporarily reduced close to z ro. particl is not subjected t such forces wh n th light irradiation is not conducted, and mov s togeth r with th flow of the dispersion m dium. Consequently, the irradiation of the light beam is repeated by turning on and off at a constant interval under the control of the control me ans (for example, the light beam on for 1 second and off for 0.1 seconds), whereby gate function with constant period can be applied to the moving fine particles. Thus, the fine particles can be moved with a desired constant spacing in the flow path behind the irradiating position 8.

More specifically, if the concentration of the fine particles in the dispersion medium is high or if the flow velocity is large, the fine particles move in succession from the supply container 1 to the irradiating position 8 as shown in Fig. 1. In such condition, the period of off-irradiation (in which the particle can pass) is made shorter than the period of on-irradiation (trapping period), so that plural particles do not pass through the irradiating position at a time. On the other hand, in the case contrary to the above-mentioned condition, there is once conducted a trapping for a long time to accumulate plural particles in front of the trapping position, and then the beam is turned on and off as explained above, thereby transferring the particles at a constant spacing.

Also, since the flow velocity of the dispersion medium is always constant, the spacing of the fine particles in movement may be arbitrarily varied by a variation in the cycle time of the light irradiation. In the condition of the off-irradiation, the irradiating light intensity need not necessarily be brought to zero, but may be reduced to a level not causing the particle trapping.

It is also possible to discriminate whether the fine particle is trapped at the irradiation position 8, by monitoring the light amount with a photosensor system positioned opposite to the light source 5 across the flow cell 3. Also, more reliable control is possible by determining the timing of irradiation, based on the monitoring.

In the case the fine particles are of a lower refractive index than that of the surrounding medium or are reflecting or absorbing the light, the trapping may be conducted by methods explained in eighth and subsequent embodiments.

[2nd embodiment]

Fig. 2 illustrates the configuration of a part of the apparatus of a second embodiment of the present invention, which is a partial modification of the embodiment shown in Fig. 1 and in which nonillustrated components are the same as those in Fig. 1.

In Fig. 2, the flow path 2 in a flow c II 12 is bent in k y-shape, and the light for optically trapping is irradiated on the flow path in front of the bent portion, in a direction along the flow path. In

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contrast to the foregoing mbodiment in which th light irradiation is mad laterally to the flow of the fine particles to trap the particles by the radial force generated by the light irradiation, the present embodiment effects the light irradiation in a direction opposite to the flow of the fine particles, thereby trapping the particle by both the axial and radial forces.

In the case the fine particles are of a lower refractive index than the surrounding medium, or ar reflecting or absorbing the light, the trapping may be achieved by methods explained in eighth and subsequent embodiments.

[3rd embodiment]

Fig. 3 shows the configuration of an apparatus constituting a third embodiment of the present invention. A supply container 20 contains particle dispersion in which a number of fine particles float in a dispersion medium. In the supply container 20 there is immersed an end of a silicone tube 21, of which the other end is connected to a flow cell 22 of quartz glass. The flow cell 22 is in turn connected to a silicone tube 23, of which the other end is connected to a nozzle 24 equipped with a micropump 25, to be explained below.

As means for forming a flow of the dispersion m dium there is employed a pump, which can be x mplified by a vacuum pump for sucking the dispersion medium from the side of the discharge container, a pressure pump for pressurizing the dispersion medium from the side of the supply container, or a feed pump having a liquid feeding m chanism. Although the vacuum pump is employed in the first embodiment, the present embodiment employs a micropump constituting a feed pump. More specifically, the micropump includes a heat-generating element provided. When a pulse voltage is given to the heat-generating element, the liquid heated by the generated heat is gasified instantaneously to generate a bubble, and liquid drops are discharged from the nozzle 24 by a pressure generated by the impact due to expansion or contraction of the bubble. The particle dispersion is sucked in toward the nozzle, corresponding to the amount of such discharge. A feeding action on the particle dispersion is obtained by effecting the discharge in consecutive manner with a high frequency to form a flow in the flow cell 22. Th fine particles move together with the flow.

Figs. 4A to 4E illustrate the mode of liquid droplet discharged by bubble generation. When the h at-generating ! m nt is heated instantaneously by a puls voltage in an initial state shown in Fig. 4A, the liquid in the vicinity of the ! m nt is gasified to g n rat a bubble as shown in Fig. 4B. Then, due to a volume expansion corresponding to

the gasification, the liquid in the vicinity of the nozzl aperture is pushed out from the aperture as shown in Fig. 4C. The bubble originally expanding starts to contract by cooling as shown in Fig. 4D, and the liquid pushed out from the aperture forms a liquid droplet and flies in the air as shown in Fig. 4E, because of the volume contraction. The liquid is replenished by capillary phenomena, corresponding to the discharged volume, whereby the initial state shown in Fig. 4A is restored. The basic principle of the liquid droplet discharging by bubble formation is detailedly described, for example, in U.S. Patent Nos. 4,732,129 and 4,740,796.

As another embodiment of the micropump, it is also possible to replace the heat-generating element with a piezoelectric element and to apply an electric pulse thereto, thereby emitting a liquid droplet by a pressure generated by the impact due to volume change of the piezoelectric element. In such case there is preferred a cylindrical piezoelement which is so provided as to surround the flow path.

The liquid feeding ability of the micropump can be selected by the voltage and frequency of the electric pulse given to the heat-generating element or the piezoelectric element. In the present embodiment the voltage and frequency supplied to the micropump 25 are so selected as to obtain a flow of the velocity in the order of 200 μ m/sec. in the flow path of the flow cell 22.

Again referring to Fig. 3, a light source 26 is composed of a YAG laser (1064 nm) for providing the fine particle with axial and radial forces, and the light for trapping the particle is condensed by a lens system 27 onto the flow path in the flow cell 22. Another light source 28 is composed of an Ar+ laser (488 nm) for measuring the optical characteristics of the fine particle, and the light for particle measurement is focused by a lens system 29 onto the flow path in the flow cell 22. The light emitted from the fine particle irradiated by the lens system 29 is collected by a lens system 30 and received by a photodetector 31 (photomultiplier or photodiode). A control means 32 effects the control of the light sources 26, 28, the analysis of the particle by the output from the photodetector 31, and the driving of the micropump 25.

When the light source 26 is turned on and the light thereof is focused on the flow path, the fine particles moving in the flow path can be trapped against the flow. When the light source is turned off, the trapping is released and the fine particle moves again together with the flow. It is therefore possibl, as in th foregoing mbodiments, t control th spacing of th fine particles s parat ly flowing one by one in the flow path, by turning on and off th irradiation of th light sourc 26 with a suitabl int rval corresponding to th flow v locity

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and the concentration of the fine particl s, under the control of the control means 32. The fine particles flowing in such array pass the irradiation position of the light sourc 28 in succession, and the light emitted from ach particle (scatt red, transmitted or fluorescent light) upon such passing is detected by the photodetector 31. The detected data are fetched by the control means 32, which ffects the analysis such as the identification of sort and property of the particles, based on the data obtained from a plurality of particles.

In the case the fine particles are of a lower refractive index than the surrounding medium, or are reflecting or absorbing the light, the trapping may be made by methods of eighth and subsequent embodiments to be explained later.

[4th embodiment]

Fig. 5 illustrates the configuration of an apparatus constituting a fourth embodiment of the present invention, in which the particle movement is achieved by the radiation pressure instead of the pump.

Referring to Fig. 5, in a cell 40 of a transparent material such as glass or plastic, there are formed a first resorvoir 41 and a second reservoir 42, which are mutually connected by paths 43, 44. Each of the paths 43, 44 has a square cross section, of which size is selected larger than the maximum diameter of a plurality of particles, but smaller than twice of the maximum diameter.

There are provided three independent laser light sources 45, 47, 49 as illustrated, and lens systems 46, 48, 50 are provided respectively, corresponding to the laser light sources. Laser beams mitted from the laser light sources 45, 47 are converted, respectively by the lens systems 46, 48, into parallel light beams (called first and second laser beams). An axial force is applied by the laser beams on the fine particles present in the light beams, in the directions of incidence of the laser beams, thereby moving the fine particles along the optical axes. Since the first and second laser beams have Gaussian intensity distribution, there can be obtained an effect that the fine particle once caught in the light beam is attracted to the optical axis by the radial force and is not released from the light beam. The first laser beam irradiating the path 43 crosses the second laser beam irradiating the path 44, and, at the crossing point, the radiation pressure of the second light beam is set larger than that of the first laser beam, so that the fine particles moved by th radiation pr ssure are smoothly moved from the path 43 to th path 44.

On the oth r hand, the laser beam emitted from the laser light source 49 is converted, by the lense system 50, into a converging light beam

(called third laser beam) condensed on the path 43, ther by providing the fine particle with a radial force for particle trapping, against the axial force of the first laser beam from the laser light source 45. In the present embodiment the third laser beam is irradiated on a position in front of the crossing point of the first and second light beams, but the third light beam may also be irradiated on the crossing point of the first and second light beams.

In the path 44 there is provided a measuring system as shown in Fig. 6, which is a view seen from the left-hand side of Fig. 5. The measured system includes, for effecting measuring light irradiation on the individually moving fine particles, a light source 52 (such as laser light source, halogen light source or xenon light source) and a lens system 53. Among the lights emitted from the irradiated fine particle, the scattered light is detected by a lens 54 and a photodetector 5 while the fluorescent light is detected by a lens 56 and a photodetector 57. The outputs from the photodetectors 55, 57 are fetched by the control means 51 for the calculation for particle analysis.

When a fine particle dispersed in the first reservoir 41 enters within the first laser beam, it is cought in the light beam and is transported in a direction A. It is thus guided to the path 43 and reach the focused position of the third laser beam. When the irradiation of the third laser beam is turned on, the fine particle stops by trapping with the light beam. When the irradiation is turned off, the trapping force is removed, whereby the fine particle starts to move again in the direction A, under the axial force by the first laser beam. When the fine particle reaches the crossing point of the first and second laser beams, it starts to move in a direction B under the stronger radiation pressure of the second laser beam, and reaches the second reservoir 42.

As in the foregoing embodiments, a control means 51 suitably selects the on-off interval of the third laser, whereby the particles move in array with a predetermined spacing in the path 44 without mutual adhesion or overlapping of the particles.

[5th embodiment]

Fig. 7 shows the configuration of an apparatus constituting a fifth embodiment, which is simplified from the configuration of the foregoing fourth embodiment. In the present embodiment, instead of the independent laser light sources in the foregoing embodiment, the light from a laser light source is split by a beam splitt r into three laser beams. Also, no path is provided for guiding th moving particles.

In a contain r 60 th r is sealed the particl dispersion similar to that in th foregoing mbodi-

ments. A light sourc 61 is composed of a YAG laser. Among the laser beams mitted therefrom, a beam transmitted by a beam splitt r 62 and a I ns 67 and split by a beam splitter 63 is further reflected by mirrors 65, 66 and introduced as the first laser beam into the container 60 (direction A). A laser beam transmitted by the beam splitter 62. lens 67 and beam splitter 63 is introduced into the container 60 as the second laser beam (direction B). Also, a laser beam emitted from the light source 61 and split by the beam splitter 62 is reflected by a mirror 64, then transmitted by a shutter 68 and focused by a lens 69 as the third laser beam onto the optical axis of the first laser beam. The positional relationship of the first, second and third laser beams is similar to that in the foregoing fourth embodiment. Also, there is provided a measuring system similar to that shown in Fig. 6 in order to optically measure the fine particles moved in array in the direction B.

The spacing in transportation of the particles is determined by on-off control of the irradiation of the third laser beam for optical trapping, through switching of the shutter 68 (liquid crystal shutter or mechanical shutter) under the control of a control means 70. The shutter may also be replaced by an optical modulation element, such as an acoustooptical element.

[6th embodiment]

Generally, assuming that intensity and the wavelength of the light for optical trapping are constant, the trapping force acting on the particle becomes larger, as the particle size increases or as the difference in refractive index between the particle and the dispersion medium becomes larger (in the case the refractive index of the particle is larger than that of the dispersion medium). Also, in the case of the same particle size, the trapping force acting thereon becomes larger, as the light intensity for optical trapping becomes stronger, or as the focused spot size of the light becomes smaller, or as the wavelength of the light becomes shorter. Consequently, the particles may be trapped or not d pending on the size or the refractive index thereof. In the following there will be explained an embodiment for separating the particles, utilizing the above-explained phenomenon, according to the size or the refractive index.

Fig. 8 illustrates the configuration of an apparatus constituting a sixth embodiment, wherein a specimen container 85 contains liquid consisting of at least two diff r nt particl s and a dispersion m dium (for example, water). Th fin particl s and dispersion medium hav c mparable specific graviti s. In th pr sent mbodim nt, the diff r nt particles are d fined to be diff rent in (1) siz, (2)

r fractiv index, or (3) siz and r fractiv index. Exampl s of the fin particl s includ cells, virus s, microorganisms, bioparticl s such as DNA or RNA, carrier particles and industrial particl s.

A container 80 contains the dispersion medium (for example, water). In the specimen container 85 and the container 80, there are respectively inserted tubes 86, 87 which are connected to a flow path 2 through a joint valve 82. The flow path 2 includes a flow cell 3 of quartz glass in the middle, and is connected to a discharge chamber 81. The chamber 81 can be maintained in a hermetically sealed condition by closing a valve 11. In the discharge chamber 81 there is provided a fraction container 88, into which the liquid having passed the flow path 2 is charged. In the above-explained configuration, the interior of the discharge chamber 81 is maintained at a low pressure by the activation of a vacuum pump 10, thereby forming a flow of the dispersion medium including the fine particles, in the flow path 2. At a downstream position of the irradiation position in the flow cell 3, there is provided particle measuring means 13 utilizing, for example, an optical, electrical, magnetic or acoustooptical method.

In the apparatus of the present embodiment, in order to set a threshold value for separating the particles according to the size or the refractive index thereof, the intensity of the trapping light beam emitting from a light source 5 and irradiated on the position 8, is rendered adjustable. This adjustment can be achieved, for example, by (1) controlling the emission intensity of the light source 5, (2) regulating the irradiating light amount by placing a modulation element or a filter in the optical path, or (3) regulating the practical light amount by varying the focused spot size at the irradiation position through adjustment of a lens 6.

The functions of the above-explained apparatus are as follows. At first, the joint valve 82 is connected to the tube 86 to introduce a small amount of the particle dispersion from the specimen container 85 into the flow path 2. Then, the joint valve 82 is switched to the tube 87, thereby introducing the dispersion medium only. Thus, the fine particles flow in the flow cell 3, together with the flow of the dispersion medium. In the irradiation position 8, a larger trapping force acts on a particle larger in size or in refractive index. In a control means 7, the irradiation intensity is set in advance by the abovementioned method at such level than the particles large in size (or in refractive index) are trapped but those small in size (or in refractive index) are not trapped. Consequ ntly, the particles larg r in siz (or in r fractiv index) alon ar trapped at th irradiation position 8, whil the smaller particles pass this position. Thus, the small r particles alon ar s I ctiv ly transmitted, th n measured by the

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measuring m ans 13 and are charged in the fraction contain r 88. Thereaft r, the fraction contain r 88 may b r covered, and the particl s trapped at th irradiation position may be measur d by flowing on by on through the control of th irradiation timing.

In the present embodiment, the threshold value for particle separation is set by adjusting the intensity of the irradiating light; but the threshold value may be varied by the wavelength of the irradiating light instead of the intensity.

[7th embodiment]

In the foregoing embodiment shown in Fig. 8, the particle separation is executed by trapping the particles completely at the irradiation position, but the separation may also be achieved by varying the moving velocity in such a manner that suitable braking force is applied to the particles according to the kind of the particle without complete trapping. In the following there will be explained such mbodiment.

Fig. 9 illustrates the configuration of an apparatus constituting a seventh embodiment of the present invention, wherein same components as those in Fig. 8 are represented by same numbers. The light emitted from the light source 5 is reflected by a mirror 91, and then separated into five beams by four half mirrors 90a, 90b, 90c, 90d and a mirror 92. The beams are respectively focused by lenses onto five positions along the flow in the flow cell 3. In the present embodiment, the reflectance/transmittance of the half mirrors 90a to 90d are so selected that the irradiation intensities are mutually equal at the irradiation positions. The irradiation intensity is maintained at such level as to not cause complete trapping of the particles. If necessary, the irradiation intensities may be made different at the irradiation positions. Also, the irradiation intensity may be made variable in order to vary the braking force.

In the above-explained configuration, when the fine particles of plural kinds different in the size or refractive index, a particle receiving a larger trapping force becomes slower in the moving velocity, receiving a larger braking force at each irradiation position. Consequently, the particles receiving smaller braking force flow faster, and the particle separation can be achieved.

[8th embodiment]

In the following ther will b xplain d a method of trapping the fine particl s in the case they are low r in the refractive index than in the surrounding medium, or they r flect or absorb the light. Fig. 10 xplains an eighthem modium not of the

pres nt invention. A laser beam 101 of Gaussian intensity distribution, emitt d from an unr presented laser light sourc (for exampl, H -N las r) nters an optical element 102 having beam splitting function. The optical element 102 is shaped as a thin cylinder whose one of faces is obliquely scraped off from the center toward a condenser lens 103 to form triangular cone. By the function of the optical element 102, the incident laser beam is split into three beams, which are focused by the condenser lens 103 as three beams 101-1, 101-2, 101-3 on a focal plane 104.

In the right-hand side of Fig. 10 there is shown a magnified view of the focal plane 104. The fine particle 105 has a lower refractive index than in the surrounding medium, or reflects or absorbs the light so that the radiation pressure functions as a repulsive force. The fine particle 105 in a position surrounded by the focal positions of three laser beams 101-1, 101-2, 101-3, cannot move from this position, because even if the particle 105 is intended to be moved outside, it is pushed back since the radiation pressures of the laser beams function as repulsive forces. Therefore, the fine particle is trapped in such position surrounded by the laser beams.

[9th embodiment]

Fig. 11 is a schematic view of a ninth embodiment of the present invention, in which the fine particles can be transported by the movement of a laser beam. A laser beam emitted from a laser light source 106 enters, through an optical pickup 108, a polarization light conversion element 109 having light splitting function, which is detailedly disclosed in Japanese Patent Laid-Open Application No. 3-191318.

The laser beam 7 entering the polarization light conversion element 109 is separated by a polarization beam splitter 109-1 into S-wave beam (reflected) and P-wave beam (transmitted). The reflected S-beam is subjected to a slight bending of the optical axis by a wedge-shaped optical element 109-2, then transmitted by a λ /4-plate 109-3, reflected by a mirror 109-4 and again transmitted by the $\lambda/4$ -plate 109-3, whereby it is converted into Pwave beam by a phase change of λ/2. This P-wave beam is transmitted by the beam splitter 109-1, then reflected by a mirror 109-5 and emerges from the lower face of the element 109. On the other hand, the P-wave beam from the incident laser beam 107 and transmitted by the beam splitter 109-1 m rg s from the low r fac of th I m nt 109. This two mirging light beams ar focus d by a lens 110 as two beams 107-1, 107-2 on a focal plan .

In such optical configuration, when th optical pickup 108 is moved by an unr presented driving mechanism in a direction of arrow perp ndicular to the optical axis, the two laser beams 107-1, 107-2 move as indicated by an arrow 111-1. Thus, a fine particle 105 is pushed by the repulsive force of the radiation pressure of the laser beams and can be moved as indicated by an arrow 111-2.

[10th embodiment]

Fig. 12 schematically shows a tenth embodiment of the present invention, in which same components as those in Fig. 11 are represented by same numbers. This embodiment is different from the configuration shown in Fig. 11 in a point that two laser light sources are used to form four beams around the fine particle. Two laser light sources 106-1, 106-2 are positioned as illustrated, and four laser beams 106-1-1, 106-1-2, 106-2-1, 106-2-2 are obtained by an optical system similar to that in Fig. 11. A fine particle 105 is trapped by th se laser beams.

As the fine particle 105 in the present embodiment is trapped by the laser beams in the surrounding four positions, it can be transported in an arbitrary three-dimensional direction by a movem nt of the optical pickup 108 in an arbitrary direction along the optical axis or perpendicular th reto, thereby three dimensionally moving the focal positions of the laser beams. Also, the fine particle may be trapped or released arbitrarily, by th on-off control of two laser light sources 106-1, 106-2.

[11th embodiment]

In the following explained is an eleventh embodiment of the present invention. In contrast to the embodiments shown in Figs. 10 to 12 which deal with one fine particle, the present embodiment can move two fine particles individually, so that, for example, two fine particles can be attached each other and fused.

In order to split a laser beam into four beams, there is employed an optical element 112 shaped as a quadrangular cone at a side as shown in Fig. 13, and the optical system is constructed similar to that in Fig. 10. Also, at the light source side on the optical axis, there is provided an optical pickup 108 which can be axially moved. Another similar optical system is symmetrically positioned on the optical axis as shown in Fig. 13, whereby two fine particles can be ind p ndently trapped and moved n the same optical axis.

In such configuration, when the two optical pickups 108 ar moved in a dir ction of th optical axis, th focal positions of the laser beams can be

axially moved, thereby moving the fin particles trapp d therein, respectively. Figs. 14A and 14B show th mod of such movem nt. Two fin particles ar mutually attached and fused by transferring from a state in Fig. 14A to a state in Fig. 14B.

[12th embodiment]

In a twelfth embodiment of the present invention explained in the following, an optical shutter 111 divided into four sectors is provided, as shown in Fig. 15, in front of a four-sectored optical element 112. The optical shutter 111 is a PLZT optical shutter, and has a circular shape split into four sectors, respectively, so as to correspond to the four faces of the quadrangular cone. It can independently turn on and off four beams on the focal plane. Two optical system of such structure are arranged side by side, as shown in Fig. 15. Each optical pickup 108 is rendered movable in a plane perpendicular to the optical axis.

Figs. 16A to 16C show the time-sequential control in the case of attaching of two fine particles. In a state shown in Fig. 16A, four beams are turned on around each particle and are so moved that the two particles approach each other. When the two particles are close to each other, the optical shutters 111 are so controlled as to turn off only a laser beam closest to the opposite particle, as shown in Fig. 16B. Thus, the two fine particles can be stably attached, as shown in Fig. 16C.

Claims

- A particle manipulating method, comprising controlling a movement of a moving particle by optically braking the moving particle.
 - A method according to claim 1, comprising controlling a movement spacing of particles by optically braking the particles.
 - A method according to claim 1, comprising separating particles by optically braking the particles.
 - 4. A particle manipulating apparatus comprising: means for moving particles; and means for irradiating toward the moving particles a light for optical braking thereof.
 - A particle measuring apparatus comprising:
 means for moving particles;
 m ans for irradiating toward moving particl s a light for optical braking ther of; and means for measuring said moving particles.

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6. A particle manipulating method comprising optically trapping a particle by focusing plural light beams ach having an intensity distribution around the particle to which radiation pressure acts as a repulsive force.

7. A method according to claim 6, comprising transporting the trapped particle by simultaneously moving focal positions of said plural light beams.

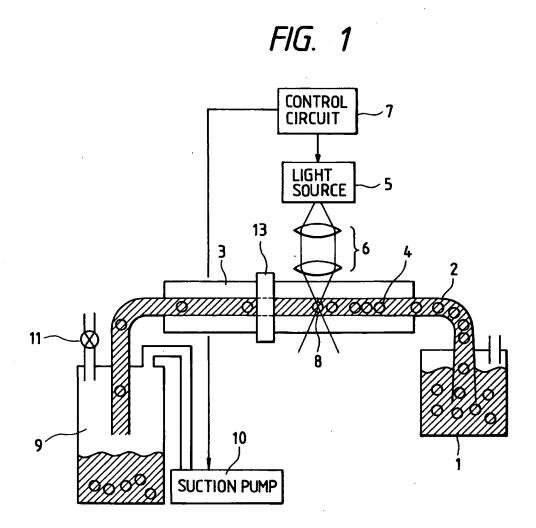


FIG. 2

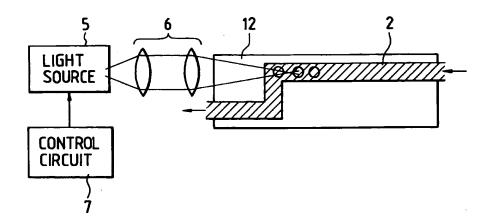
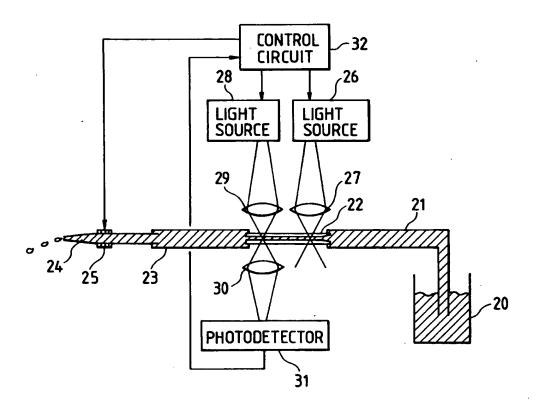
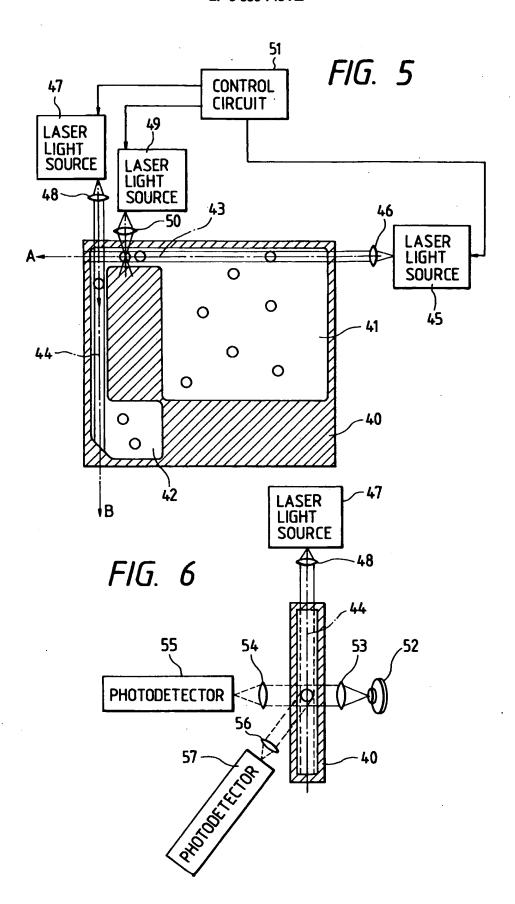
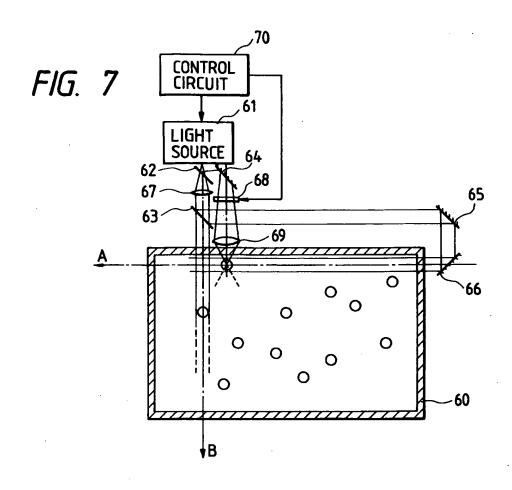


FIG. 3









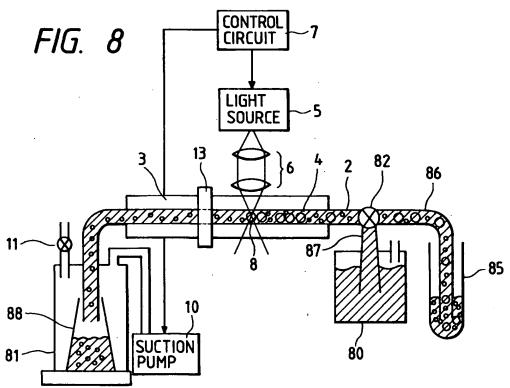
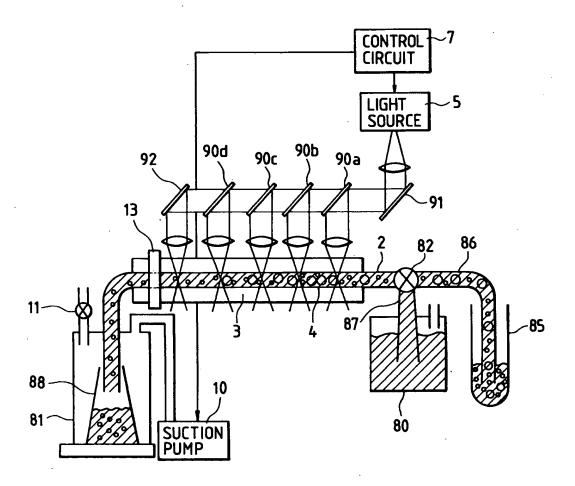
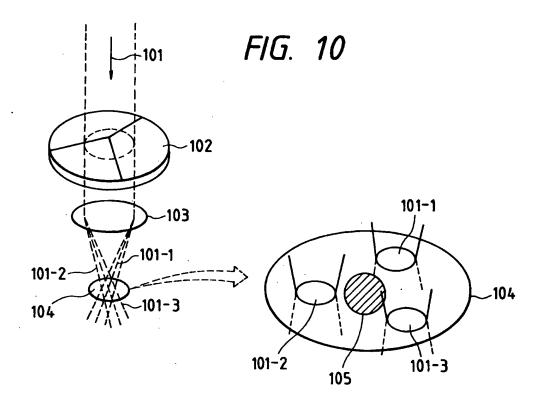


FIG. 9





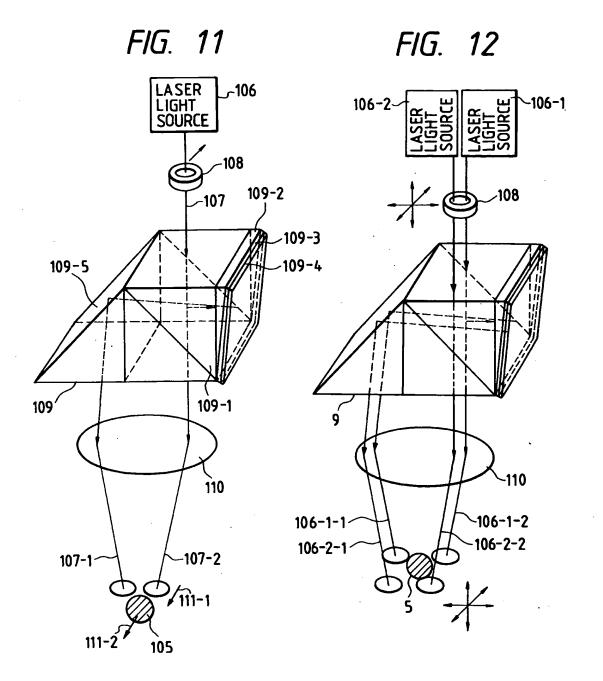


FIG. 13

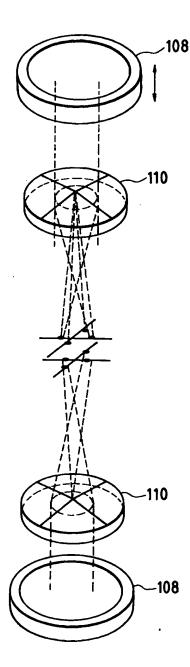


FIG. 15

